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Fast E-BEM by ACA compression for the resolution of acoustic and elastic 2D exterior problems in time domain

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# MOTIVATIONS and OUTLINE OF THE TALK



- 1. Acoustics and Elastic model problems (soft scattering)
- 2. Energetic Boundary Element Method (E-BEM)
- 3. ACA based E-BEM reduction of computational costs and memory requirements
- 4. Numerical results
- 5. Ongoing research

• Wave propagation into a linear, homogeneous and isotropic unbounded domain  $\Omega_e \subset \mathbb{R}^2$ :



 $\Omega_e = \mathbb{R}^2 \setminus \overline{\Omega}$ 

Scattering by a closed domain  $\boldsymbol{\Omega}$ 

# Acoustic Parameters $\rho$ mass densityc wave propagation speedElastic Parameters $\rho$ mass density $\lambda$ Lamé parameter

 $\mu$  shear modulus



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• We consider an indirect boundary integral representation formula for **u** in  $\Omega_e \times (0, T]$ :

 $\mathbf{u}(\mathbf{x},t) = \mathbf{V} \Phi (\mathbf{x},t) = \int_{\Gamma} \mathbf{G}^{\mathbf{u}\mathbf{u}}(\mathbf{x}-\mathbf{y};t) \star^{(t)} \Phi(\mathbf{y},t) d\Gamma_{\mathbf{y}}, \qquad (\mathbf{x},t) \in \Omega_{e} \times (0,T]$   $\Phi \text{ is an unknown density field belonging to the functional space of the traction vector } \mathbf{p} = (p_{1},p_{2})^{\mathsf{T}}:$   $p_{i}(\mathbf{x},t) = \sum_{h=1}^{2} \sigma_{ih}[\mathbf{u}](\mathbf{x},t)n_{h}(\mathbf{x}), i = 1,2$ 

# 1. ACOUSTIC and ELASTIC MODEL PROBLEMS (SOFT SCATTERING)

# BOUNDARY INTEGRAL EQUATION

• The integral representation formula is strictly connected to the definition of the 2D fundamental solution  $\mathbf{G}^{\mathbf{u}\mathbf{u}} = (G_{ij}^{\mathbf{u}\mathbf{u}})_{i,j=1,2}$ :

$$G_{ij}^{uu}(\mathbf{x} - \mathbf{y}; t - \tau) = \underbrace{\text{elastodynamics}}_{r = \mathbf{x} - \mathbf{y}, r = ||\mathbf{x} - \mathbf{y}||}^{k(u)} \left( \frac{\mathbf{x} - \mathbf{y}; t - \tau}{\mathbf{y}; t - \tau} \right) = \underbrace{\frac{\mathbf{y} - \mathbf{y}}{\mathbf{y}; t - \tau}}_{r = \mathbf{x} - \mathbf{y}, r = ||\mathbf{x} - \mathbf{y}||}^{k(u)} \left( \frac{\mathbf{y} - \mathbf{y}}{\mathbf{y}; t - \tau} \right) = \underbrace{\frac{\mathbf{y} - \mathbf{y}}{\mathbf{y}; t - \tau}}_{r = \mathbf{x} - \mathbf{y}, r = ||\mathbf{x} - \mathbf{y}||}^{k(u)} \left( \frac{\mathbf{y} - \mathbf{y}}{\mathbf{y}; t - \tau} \right) = \underbrace{\frac{\mathbf{y} - \mathbf{y}}{\mathbf{y}; t - \tau}}_{r = \mathbf{x} - \mathbf{y}, r = ||\mathbf{x} - \mathbf{y}||}^{k(u)} \left( \frac{\mathbf{y} - \mathbf{y}}{\mathbf{y}; t - \tau} \right) = \underbrace{\frac{\mathbf{y} - \mathbf{y}}{\mathbf{y}; t - \tau}}_{r = \mathbf{y} - \mathbf{y}, r = ||\mathbf{x} - \mathbf{y}||}^{k(u)} \left( \frac{\mathbf{y} - \mathbf{y}}{\mathbf{y}; t - \tau} \right) = \underbrace{\frac{\mathbf{y} - \mathbf{y}}{\mathbf{y}; t - \tau}}_{r = \mathbf{y} - \mathbf{y}, r = ||\mathbf{x} - \mathbf{y}||}^{k(u)} \left( \frac{\mathbf{y} - \mathbf{y}}{\mathbf{y}; t - \tau} \right) = \underbrace{\frac{\mathbf{y} - \mathbf{y}}{\mathbf{y}; t - \tau}}_{r = \mathbf{y} - \mathbf{y}, r = ||\mathbf{y} - \mathbf{y}||}^{k(u)} \left( \frac{\mathbf{y} - \mathbf{y}}{\mathbf{y}; t - \tau} \right) = \underbrace{\frac{\mathbf{y} - \mathbf{y}}{\mathbf{y}; t - \tau}}_{r = \mathbf{y} - \mathbf{y}, r = ||\mathbf{y} - \mathbf{y}||}^{k(u)} \left( \frac{\mathbf{y} - \mathbf{y}}{\mathbf{y}; t - \tau} \right) = \underbrace{\frac{\mathbf{y} - \mathbf{y}}{\mathbf{y}; t - \tau}}_{r = \mathbf{y} - \mathbf{y}, r = ||\mathbf{y} - \mathbf{y}||}^{k(u)} \left( \frac{\mathbf{y} - \mathbf{y}}{\mathbf{y}; t - \tau} \right) = \underbrace{\frac{\mathbf{y} - \mathbf{y}}{\mathbf{y}; t - \tau}}_{r = \mathbf{y} - \mathbf{y}, r = ||\mathbf{y} - \mathbf{y}||}^{k(u)} \left( \frac{\mathbf{y} - \mathbf{y}}{\mathbf{y}; t - \tau} \right) = \underbrace{\frac{\mathbf{y} - \mathbf{y}}{\mathbf{y}; t - \tau}}_{r = \mathbf{y} - \mathbf{y}, r = ||\mathbf{y} - \mathbf{y}||}^{k(u)} \left( \frac{\mathbf{y} - \mathbf{y}}{\mathbf{y}; t - \tau} \right) = \underbrace{\frac{\mathbf{y} - \mathbf{y}}{\mathbf{y}; t - \tau}}_{r = \mathbf{y} - \mathbf{y}, r = ||\mathbf{y} - \mathbf{y}||}^{k(u)} \left( \frac{\mathbf{y} - \mathbf{y}}{\mathbf{y}; t - \tau} \right) = \underbrace{\frac{\mathbf{y} - \mathbf{y}}{\mathbf{y}; t - \tau}}_{r = \mathbf{y} - \mathbf{y}, r = ||\mathbf{y} - \mathbf{y}||}^{k(u)} \left( \frac{\mathbf{y} - \mathbf{y}}{\mathbf{y}; t - \tau} \right) = \underbrace{\frac{\mathbf{y} - \mathbf{y}}{\mathbf{y}; t - \tau}}_{r = \mathbf{y} - \mathbf{y}, r = ||\mathbf{y} - \mathbf{y}|}^{k(u)} \left( \frac{\mathbf{y} - \mathbf{y}}{\mathbf{y}; t - \tau} \right) = \underbrace{\frac{\mathbf{y} - \mathbf{y}}{\mathbf{y}; t - \tau}}_{r = \mathbf{y} - \mathbf{y}, r = ||\mathbf{y} - \mathbf{y}|}^{k(u)} \left( \frac{\mathbf{y} - \mathbf{y}}{\mathbf{y}; t - \tau} \right) = \underbrace{\frac{\mathbf{y} - \mathbf{y}}{\mathbf{y}; t - \tau}}_{r = \mathbf{y} - \mathbf{y}, r = ||\mathbf{y} - \mathbf{y}|}^{k(u)} \left( \frac{\mathbf{y} - \mathbf{y}}{\mathbf{y}; t - \tau} \right) = \underbrace{\frac{\mathbf{y} - \mathbf{y}}{\mathbf{y}; t - \tau}}_{r = \mathbf{y} - \mathbf{y}$$

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• Performing a limiting process of the spatial variable from the domain to the boundary, we get to the Boundary Integral Equation (BIE):

$$\mathbf{u}(\mathbf{x},t) = \mathbf{V}\mathbf{\Phi}(\mathbf{x},t), \mathbf{x} \in \Omega_e, t \in (0,T]$$
  
representation formula  
$$\mathbf{x} \in \Omega_e \to \mathbf{x} \in \Gamma$$
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BIE

• Standard discretization of the BIE may lead to unstable results for the approximation of the BIE unknown:



A. Frangi et al., On the numerical stability of time-domain elastodynamic analyses by BEM, CMAME, 1999

# BOUNDARY INTEGRAL EQUATION and ITS ENERGETIC WEAK FORMULATION

• BIE in the unknown density **Φ**:

 $\nabla \mathbf{\Phi} (\mathbf{x}, t) = \mathbf{g}_{\mathcal{D}} (\mathbf{x}, t), \quad \mathbf{x} \in \Gamma, t \in (0, T]$ 

• Energetic Weak Formulation: find  $\Phi \in H^0[(0,T); H^{-1/2}(\Gamma)]$  solution of the energetic weak problem

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- The link with the energy  $\mathcal{E}$  of the system allows to obtain good theoretical properties  $[\mathbf{z}]$  for the bilinear form  $B_{\mathcal{D}}(\mathbf{\phi}, \mathbf{\phi})$ .
- This energetic approach allows to overcome the instabilities arising from the standard weak form of the BIEs.

# 2. ENERGETIC BOUNDARY ELEMENT METHOD (E-BEM)



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• Block forward substitution process to obtain the solution:

$$\mathbb{E}_{V}^{(0)}\boldsymbol{\alpha}_{(l)} = \boldsymbol{z}_{(l)} \qquad \forall l = 0, \dots, N \qquad \text{where} \qquad \boldsymbol{z}_{(l)} = \boldsymbol{\beta}_{(l)} - \sum_{j=1}^{l} \mathbb{E}_{V}^{(j)} \boldsymbol{\alpha}_{(l-j)},$$

- ✓ only the non-singular block  $\mathbb{E}_V^{(0)}$  has to be inverted.
- ✓ for each l = 1,...,N-1, the time blocks  $\mathbb{E}_V^{(l)}$  are used to update the RHS at each time step
- × for growing time, i.e. for growing index *l*, depending on wave speeds, blocks become fully populated *O(NM<sup>2</sup>)* overall cost
- × for large *M* the updating of the RHS is expensive in terms of computations and memory requirements!

we need a compression technique to reduce the overall cost

ENTRIES of the ACOUSTICS TIME BLOCKS

$$\mathbb{E}_{V}^{(l)} = \begin{pmatrix} \mathbb{E}^{(l)} & 0 \\ 0 & \mathbb{E}^{(l)} \end{pmatrix} \quad l = 0, \dots, N-1 \quad \text{structure of the acoustic time block}$$
  
dimension  $2M \times 2M$ 

• After a double analytic integration in the time variables, the entries of a generic acoustic block are expressed as follows:

$$\left(\mathbb{E}^{(l)}\right)_{\widetilde{m},m} = -\sum_{\zeta,\xi=0}^{1} \frac{(-1)^{\xi+\zeta}}{2\pi} \int_{\Gamma} \int_{\Gamma} w_{\widetilde{m}}^{p}(\mathbf{x}) \ w_{m}^{p}(\mathbf{y}) \ \nu(r;\Delta_{h+\xi,k+\zeta}) d\Gamma_{\mathbf{y}} d\Gamma_{\mathbf{x}}, \qquad \Delta_{h,k} = t_{h} - t_{k}$$

with

$$\nu(r;\Delta) = H[c\Delta - r] \left[ \log \left( c\Delta + \sqrt{c^2 \Delta^2 - r^2} \right) - \log(r) \right] \qquad \qquad \text{singularity of type} \\ \mathcal{O}(\log(r)) \text{ for } r \to 0$$

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• **FUNDAMENTAL REMARK**: if we set  $\Delta_{hk} = t_l$ , for growing time we have  $ct_{l+1} > r$  and the block entries reduce to

$$\left(\mathbb{E}^{(l)}\right)_{\widetilde{m},m} = -\frac{1}{2\pi} \int_{\Gamma} \int_{\Gamma} w_{\widetilde{m}}^{\mathbf{p}}(\mathbf{x}) w_{m}^{\mathbf{p}}(\mathbf{y}) \widetilde{\nu}(r;t_{l}) d\Gamma_{\mathbf{y}} d\Gamma_{\mathbf{x}},$$

where the new compact kernel is

$$\tilde{\nu}(r,t) = \log\left(\frac{\left(ct + \sqrt{c^2t^2 - r^2}\right)^2}{\left(c(t - \Delta t) + \sqrt{c^2(t - \Delta t)^2 - r^2}\right)\left(c(t + \Delta t) + \sqrt{c^2(t + \Delta t)^2 - r^2}\right)}\right)$$

and we do not observe any singularity since now the kernel is smooth for  $r \to 0$ . Moreover,  $\tilde{v}(r,t) \to 0$  for  $t \to +\infty$  and it is symmetric in space variables.

# LOW-RANK REPRESENTATION of the TIME INTEGRATED ACOUSTICS KERNEL

• The reduction of the memory storage of the energetic BEM is related to the possibility of writing a low-rank representation or degenerate expansion of the kernel function, i.e.

$$\tilde{\nu}(\mathbf{x}, \mathbf{y}; t_l) = \sum_{k=0}^{k_l^*} \chi_k(\mathbf{x}, t_l) \omega_k(\mathbf{y}, t_l) + R_{k_l^*}(\mathbf{x}, \mathbf{y}, t_l),$$

where  $R_{k_l^*}(\mathbf{x}, \mathbf{y}; t_l)$  is the residuum that tends to zero for  $k_l^* \to \infty$ . It is well known that a kernel with the properties of  $\tilde{v}$  possesses a low-rank representation in terms of eigenvalues and eigenfunctions in space variables  $\exists$ ; however this is not useful to get to a closed form for this representation allowing to estimate the residuum with respect to a set rank  $k_l^*$ .

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• Estimate of the low-rank: we consider a Taylor expansion in the  $r = ||\mathbf{x} - \mathbf{y}||$  variable, centered in r = 0:

$$\tilde{v}(r,t_l) = \sum_{k=0}^{k_l^*} C_k(t_l) r^{2k} + R_{k_l^*}(r,t_l) \coloneqq S_{k_l^*}(r,t_l) + R_{k_l^*}(r,t_l),$$

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$$C_k(t_l) \cong (\Delta tc)^2 \frac{(2k+1)!}{(k!)^2 4^k} \frac{1}{(ct_l)^{2k+2}}.$$

Hence

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$$= \Delta t^2 c \frac{\partial^2}{\partial t_l \partial r} \left[ \sum_{k=0}^{k_l^*} \frac{(2k)!}{(2k+1)! (k!)^2 4^k} \left(\frac{r}{ct_l}\right)^2 \right]$$

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# LOW-RANK REPRESENTATION of ACOUSTICS BLOCKS

• Thus, for  $k_l^* \to \infty$  we have:

$$\tilde{\nu}(r,t_l) \simeq \tilde{S}_{\infty}(r,t_l) = c\Delta t^2 \left( \frac{1}{t_l (c^2 t_l^2 - r^2)^{1/2}} + \frac{r^2}{t_l (c^2 t_l^2 - r^2)^{3/2}} \right)$$

We can conclude that it is possible to obtain a low-rank approximation of  $\tilde{v}(r, t_l)$  and  $k_l^*$  is the rank required to achieve a given relative accuracy  $\varepsilon > 0$  if

$$\left|R_{k_l^*}(r,t_l)\right| \simeq \left|\tilde{S}_{\infty}(r,t_l) - \tilde{S}_{k_l^*}(r,t_l)\right| \le \varepsilon \left|\tilde{S}_{\infty}(r,t_l)\right|$$

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• At the discrete level, the low rank representation of the kernel  $\tilde{v}(r, t_l)$  implies that

$$\mathbb{E}^{(l)} = \mathbb{S}_{k_l^*} + \mathbb{R}_{k_l^*} \text{ with } \mathbb{S}_{k_l^*} = \mathbb{Q} \cdot \mathbb{W}^{\mathsf{T}}$$

where  $\mathbb{Q}$  and  $\mathbb{W}$  are both  $M \times k_l^*$  matrices and the residuum  $\mathbb{R}_{k_l^*}$  is such that:

$$\left\| \mathbb{R}_{k_{l}^{*}} \right\|_{F} = \left\| \mathbb{E}^{(l)} - \mathbb{S}_{k_{l}^{*}} \right\|_{F} = \left\| \mathbb{E}^{(l)} - \mathbb{Q} \cdot \mathbb{W}^{\mathsf{T}} \right\|_{F} \le \varepsilon \left\| \mathbb{E}^{(l)} \right\|_{F}$$

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• Remark. For  $k_l^* \ll M$  we obtain a drastic reduction of the memory requirement for the storage of  $\mathbb{E}^{(l)}$ .

How to compute the matrices  $\mathbb{Q}$  and  $\mathbb{W}$ ?

# ACA ALGORITHM FOR THE LOW-RANK APPROXIMATIONS OF ACOUSTICS BLOCKS

• Truncated SVD:

$$\mathbb{E}^{(l)} \simeq \sum_{k=0}^{k_l^*} \mathbf{q}_k \sigma_k \mathbf{w}_k^{\mathsf{T}} = \mathbb{Q} \Sigma \mathbb{W}^{\mathsf{T}}$$

- ✓ gives the best low-rank approximation
- × requires the evaluation of all entries
- × cost of the algorithm:  $\mathcal{O}(M^3)$

### ACA based E-BEM 3.

# ACA ALGORITHM FOR THE LOW-RANK APPROXIMATIONS OF ACOUSTICS BLOCKS

Truncated SVD: •

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$$\mathbb{E}^{(l)} \simeq \sum_{k=0}^{k_l^*} \mathbf{q}_k \sigma_k \mathbf{w}_k^{\mathsf{T}} = \mathbb{Q} \Sigma \mathbb{W}^{\mathsf{T}}$$

- gives the best low-rank approximation  $\checkmark$
- requires the evaluation of all entries Х
- cost of the algorithm:  $O(M^3)$ Х
- Efficient algorithm to compute the low-rank approximations: •

partially pivoted Adaptative Cross Approximation ; it basically consists in the computation of successive rank-1 approximations

$$\mathbb{E}^{(l)} = \mathbb{S}_{k_l^*} + \mathbb{R}_{k_l^*}, \qquad \mathbb{R}_{k_l^*} = \mathbb{E}^{(l)} - \sum_{k=1}^{k_l^*} \mathbf{q}_k \mathbf{w}_k^{\mathsf{T}}$$

- requires only few entries of the matrix in practice,  $O(k_l^*M)$  complexity  $\checkmark$ 
  - M. Bebendorf and S. Rjasanow, Computing, (2003)



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# ACA ALGORITHM FOR THE LOW-RANK APPROXIMATIONS OF ACOUSTICS BLOCKS

• Truncated SVD:

$$\mathbb{E}^{(l)} \simeq \sum_{k=0}^{k_l^*} \mathbf{q}_k \sigma_k \mathbf{w}_k^{\mathsf{T}} = \mathbb{Q} \Sigma \mathbb{W}^{\mathsf{T}}$$

- gives the best low-rank approximation
- X requires the evaluation of all entries
- X cost of the algorithm:  $\mathcal{O}(M^3)$
- Efficient algorithm to compute the low-rank approximations:

partially pivoted Adaptative Cross Approximation  $\exists$ ; it basically consists in the computation of successive rank-1 approximations of  $\mathbb{E}^{(l)}$ :

$$\mathbb{E}^{(l)} = \mathbb{S}_{k_l^*} + \mathbb{R}_{k_l^*}, \qquad \mathbb{R}_{k_l^*} = \mathbb{E}^{(l)} - \sum_{k=1}^{k_l^*} \mathbf{q}_k \mathbf{w}_k^{\mathsf{T}}$$



✓ requires only few entries of the matrix
✓ in practice, O(k<sub>l</sub><sup>\*</sup>M) complexity

M. Bebendorf and S. Rjasanow, Computing, (2003)

Computational cost of the ACA based Energetic BEM: if  $ct_{l^*} > \sqrt{3}diam(\Gamma)$ , for any fixed  $\varepsilon > 0$  and  $l > l^*$ , the rank of the block  $\mathbb{E}^{(l)}$  can be bounded from above by the solution  $k^*(\varepsilon)$  of the following inequality:

$$\frac{2(2k+3)!}{[(k+1)!]^2 1 2^{k+1}} < \varepsilon$$

the ACA based compression scheme is bounded from the above by  $2 k^*(\varepsilon)(1 - \lambda)NM$ , where  $\lambda = \frac{\sqrt{3}diam(\Gamma)}{cT}$ 

ENTRIES of the ELASTODYNAMICS TIME BLOCKS

$$\mathbb{E}_{V}^{(l)} = \begin{pmatrix} \mathbb{E}_{V,11}^{(l)} & \mathbb{E}_{V,12}^{(l)} \\ \mathbb{E}_{V,21}^{(l)} & \mathbb{E}_{V,22}^{(l)} \end{pmatrix} \quad l = 0, \dots, N$$

structure of the elastodynamic time block

dimension  $2M \times 2M$ 

• After a double analytic integration in the time variables, the entries of a generic elastodynamic block are expressed as follows:

$$\left(\mathbb{E}^{(l)}\right)_{\widetilde{m},m} = -\sum_{\zeta,\xi=0}^{1} \frac{(-1)^{\xi+\zeta}}{2\pi\rho} \int_{\Gamma} \int_{\Gamma} w_{\widetilde{m}}^{p}(\mathbf{x}) w_{m}^{p}(\mathbf{y}) \nu(r;\Delta_{h+\xi,k+\zeta}) d\Gamma_{\mathbf{y}} d\Gamma_{\mathbf{x}}, \quad \Delta_{h,k} = t_{h} - t_{k}$$

with

- 1

having set

$$\varphi_{\gamma}(r;\Delta) = c_{\gamma} \Delta \sqrt{c_{\gamma}^2 \Delta^2 - r^2}, \qquad \hat{\varphi}_{\gamma}(r;\Delta) = \log \left( c_{\gamma} \Delta + \sqrt{c_{\gamma}^2 \Delta^2 - r^2} \right) - \log(r)$$

- Having set  $\Delta_{hk} = t_l$ , for growing time we have  $ct_{l+1} > r$  and in the above sum singularity disappears.
- The previously applied block low-rank ACA approximation procedure can be applied also in the elastodynamics context

# ACOUSTICS: EFFICIENCY and ACCURACY

Boundary datum: 
$$g_{\mathcal{D},1}(x,t) = t^4 e^{-t} \cos(x_1^2 + 2x_2^2)$$
 and  $g_{\mathcal{D},2}(x,t) = 0$   
Threshold:  $\varepsilon_{ACA} = 1.0e - 04$ 

Absolute Error: 
$$E_{L^2} \coloneqq \max_{t \in (0,T]} \left\| \Phi_{M_e,N_e}^*(\cdot,t) - \Phi_{M,N}(\cdot,t) \right\|_{L^2(\Gamma)}$$
  $(M_e = 4096, N_e = 8192, T = 4\pi)$   
Memory Saving:  $mem(\%) \coloneqq 100 \cdot \left(1 - \frac{1}{N} \sum_{l=0}^{N-1} \frac{2k_l^*}{M}\right)$ 

			C = 1			C = 343	
М	Ν	$E_{L^2}$	EOC	mem(%)	$E_{L^2}$	EOC	mem(%)
8	16	2.67 <i>e</i> – 01	0.6	0.0%	5.94 <i>e –</i> 01	0.7	37.5%
16	32	1.77 <i>e –</i> 01	1.0	0.0%	3.54 <i>e –</i> 01	1.0	67.2%
32	64	8.47 <i>e</i> – 02	1.0	39.0%	1.78 <i>e –</i> 01	1.0	84.6%
64	128	4.22 <i>e</i> – 02	1.0	60.9%	8.95 <i>e –</i> 02	1.0	92.1%
128	256	2.03 <i>e</i> – 02	1.1	72.1%	4.41 <i>e</i> – 02	1.0	96.0%
256	512	9.44 <i>e</i> – 03	1.2	77.3%	2.13 <i>e</i> – 02	1.1	96.0%
512	1024	4.04 <i>e</i> – 03		79.7%	9.93 <i>e</i> – 03		98.3%



*x*<sub>2</sub>

 $x_1$ 

 $\pi^{\overline{2}}$ 

ACOUSTICS: SAVING of CPU TIME and GLOBAL TIME HISTORY of the ERROR

# **CPU TIME**

The growth of the CPU time (measured in seconds) with ACA compression is optimal, i.e. O(NM).

# TIME HISTORY OF THE ERROR

$$E_{L^{2}}(t) \coloneqq \left\| \Phi_{M_{e},N_{e}}^{*}(\cdot,t) - \Phi_{M,N}(\cdot,t) \right\|_{L^{2}(\Gamma)}$$
  
(M<sub>e</sub> = M = 4096, N<sub>e</sub> = N = 8192)

For growing time, the level of error introduced by the ACA can be controlled by the parameter  $\varepsilon_{ACA}$ , since the former is at most of the same order of magnitude of the latter.





# **ACOUSTICS: APPLICATION to SCATTERING PROBLEMS**

• Scattering of a packet of four plane waves impacting on a circumference of radius 1

Boundary datum:  $g_{D,1}(x,t) = -\sum_{i=1}^{4} e^{(-2(x_1 - \xi_i + c(t+t_0))^2)}$  and  $g_{D,2}(x,t) = 0$ ; Parameters:  $\xi = (50,55,60,65)^{\mathsf{T}}$ ,  $t_0 = 0.13$ , c = 343 and T = 0.15DOF: M = 128 and N = 1049, Threshold:  $\varepsilon_{ACA} = 1.0e - 04 \Longrightarrow mem(\%) = 87.3$ 

• Representation of the horizontal component of the reconstructed total field in a region surrounding the scatterer



# ACOUSTICS: APPLICATION to SCATTERING PROBLEMS

• Scattering of a plane wave impinging on a flower-shaped scatterer

Boundary datum:  $g_{D,1}(x,t) = e^{(-50(x_1-50+c(t+0.13))^2)}$  and  $g_{D,2}(x,t) = 0$ ; Parameters: c = 343 and T = 0.07DOF: M = 4096 and N = 10352Threshold:  $\varepsilon_{ACA} = 1.0e - 04 \implies mem(\%) = 86.2$ 

• Representation of the horizontal component of the reconstructed total field in a region surrounding the scatterer



## ELASTODYNAMICS: EFFICIENCY and ACCURACY

Boundary datum: 
$$g_{D,1}(x,t) = t^4 e^{-t} x_1$$
 and  $g_{D2}(x,t) = t^4 e^{-t} x_2$ ;  
Threshold:  $\varepsilon_{ACA} = 1.0e - 04$ 

Absolute Error:  $E_{L^2} \coloneqq_{t \in (0,T]} \left\| \Phi_{M_e,N_e}^*(\cdot,t) - \Phi_{M,N}(\cdot,t) \right\|_{L^2(\Gamma)}$   $(M_e = 512, N_e = 2048, T = 4\pi)$ Memory Saving:  $mem(\%) \coloneqq 100 \cdot \left( 1 - \frac{1}{N} \sum_{ij=1}^{2} \sum_{l=0}^{N-1} \frac{2k_{ij,l}^*}{M} \right)$ 

		C <sub>s</sub>	$s_{s} = 1, C_{P} =$	2
М	Ν	$E_{L^2}$	EOC	mem(%)
8	32	6.29e-01	1.0	0.0%
16	64	3.11e-01	1.1	0.0%
32	128	1.49e-01	1.2	38.7%
64	256	6.44e-02	1.5	60.2%
128	512	2.15e-02		71.0%



-2

 $\alpha \in (-\pi,\pi]$ 

0

2

10

15

 $t\in [0,4\pi]$ 

# **ELASTODYNAMICS: APPLICATION to SCATTERING PROBLEMS**

• Scattering of an incident P-wave impacting on a circumference of radius 1

Boundary datum:  $g_{D,1}(x,t) = e^{(-20(x_1-2+c_Pt-0.475)^2)}$  and  $g_{D,2}(x,t) = 0$ Parameters:  $c_S = 1$ ,  $c_P = \sqrt{3}$  and T = 12DOF: M = 128 and N = 426Threshold:  $\varepsilon_{ACA} = 1.0e - 04 \Longrightarrow mem(\%) = 71.1$ 

• Representation of the horizontal and vertical components of the reconstructed total field in a region surrounding the scatterer



# **ELASTODYNAMICS: APPLICATION to SCATTERING PROBLEMS**

• Scattering of an incident P-wave impacting on a kite-shaped scatterer

Boundary datum:  $g_{D,1}(x,t) = e^{(-20(x_1 - 2 + c_P t - 0.475)^2)}$  and  $g_{D,2}(x,t) = 0$ ; Parameters:  $c_S = 1, c_P = \sqrt{3}$  and T = 12DOF: M = 8192 and N = 28380Threshold:  $\varepsilon_{ACA} = 1.0e - 04 \implies mem(\%) = 72.5$ 

• Representation of the horizontal and vertical components of the reconstructed total field in a region surrounding the scatterer



# 5. ONGOING RESEARCH

# ACOUSTIC and ELASTIC HARD SCATTERING PROBLEMS

• PDE:  $\rho \ddot{\mathbf{u}}(\mathbf{x},t) - \nabla \cdot \sigma [\mathbf{u}](\mathbf{x},t) = 0, \qquad (\mathbf{x},t) \in \Omega_e \times (0,T]$  $\begin{cases} \mathbf{u}(\mathbf{x},0) = \dot{\mathbf{u}}(\mathbf{x},0) = 0, & \mathbf{x} \in \Omega_e \\ \mathbf{p}(\mathbf{x},t) = \mathbf{g}_N(\mathbf{x},t), & (\mathbf{x},t) \in \Gamma \times (0,T] \end{cases}$ 

• BIE:  $\mathbf{g}_N(\mathbf{x},t) = W \mathbf{\psi}(\mathbf{x},t), \qquad \mathbf{x} \in \Gamma, t \in (0,T]$ where  $W \mathbf{\psi}(\mathbf{x},t) = \int_{\Gamma} \mathbf{G}^{\mathbf{pp}}(\mathbf{x} - \mathbf{y};t) \star^{(t)} \mathbf{\psi}(\mathbf{y},t) d\Gamma_{\mathbf{y}}, \qquad \text{with} \qquad \mathbf{G}^{\mathbf{pp}}(\mathbf{x} - \mathbf{y};t) = \sigma_{\mathbf{x}}[\sigma_{\mathbf{y}}[\mathbf{G}^{\mathbf{uu}}]]$ 

• Energetic BEM:  $\mathbb{E}_W \boldsymbol{a} = \boldsymbol{\beta}$  Toeplitz block lower triangular matrix

- After a double analytic integration in the time variables, the entries of a generic time block are double integrals over  $\Gamma \times \Gamma$ , whose kernel has a hyper-singularity of type  $O(1/r^2)$  for  $r \to 0$
- For growing time, the kernel singularity disappears and time blocks are vanishing with decreasing rank.
- The previously applied block low-rank ACA approximation procedure can be applied also in the context of hard scattering.

# 5. ONGOING RESEARCH

# ACOUSTICS AND ELASTODYNAMICS HARD SCATTERING : EFFICIENCY and ACCURACY

(Components of the) Boundary datum on a rectilinear scatterer of unitary length:  $g_{\mathcal{N},1}(x,t) = g_{\mathcal{N},2}(x,t) = H[t]$ ;

Threshold:  $\varepsilon_{ACA} = 1.0e - 04$ 

Absolute error evaluated in energy norm

Memory Saving: 
$$mem(\%) \coloneqq 100 \cdot \left(1 - \frac{1}{N} \sum_{l=0}^{N-1} \frac{2k_l^*}{M}\right)$$

T = 5		$\begin{array}{l} \textbf{Acoustics} \\ (c_S = 1) \end{array}$			<b>Elastodynamics</b> $(c_S = 1, c_P = 2)$		
М	Ν	Ε	ЕОС	mem(%)	Ε	ЕОС	mem(%)
9	50, 100	1.93 <i>e</i> – 01	0.5	0.0%	2.27 <i>e</i> – 01	0.5	0.0%
19	100, 200	1.37 <i>e</i> – 01	0.5	11.2%	1.59e — 01	0.5	41.2%
39	200, 400	9.59 <i>e</i> — 02	0.5	31.2%	1.12e – 01	0.5	59.7%
79	400, 800	6.70 <i>e</i> – 02	0.5	50.2%	7.91 <i>e –</i> 02	0.5	69.8%
159	800, 1600	4.71 <i>e</i> – 02		64.7%	5.50 <i>e –</i> 02		75.9%



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# THANK YOU FOR THE ATTENTION AND... HAPPY BIRTHDAY ERNST STEPHAN!

